



U. of Montana

Self-Consistent Cross Phase Evolution

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Goals of this work

- Develop an evolution equation for the cross phase
- Use this equation in a self-consistent model for the L-H transition
- Estimate the effects on power thresholds and transition dynamics

*The **cross phase**, δ , between radial velocity and density (or temperature) fluctuations affects:*

- turbulent transport of particles (or heat)
- rates of nonlinear energy transfer due to the $E \times B$ nonlinearity
- timing of and threshold for L-H transitions in phase transition models

- Consider the cross phase between density and radial velocity fluctuations:

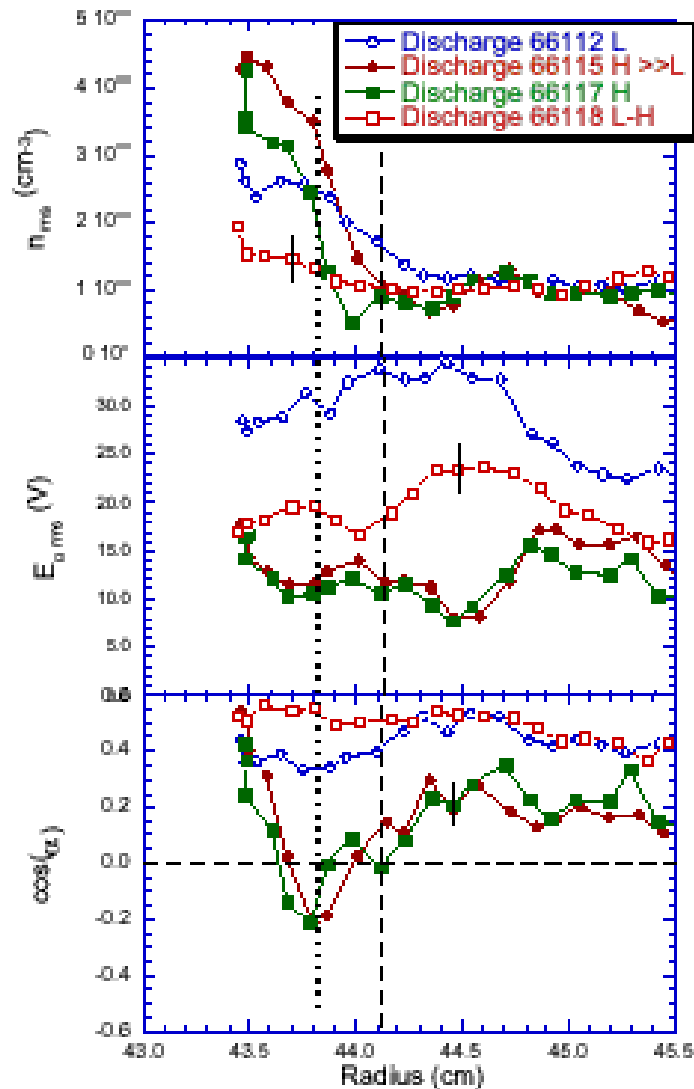
$$= \langle \tilde{v}_r^* \tilde{n} \rangle = \langle \tilde{v}_r^2 \rangle^{1/2} \langle \tilde{n}^2 \rangle^{1/2} C_{v,n} \cos()$$

- $C_{v,n}$ is the coherence (assume ~ 1)
- $\cos()$ is the cross phase

$$\cos = \frac{\langle \tilde{v}_r^* \tilde{n} \rangle}{\langle \tilde{v}_r^2 \rangle^{1/2} \langle \tilde{n}^2 \rangle^{1/2}}$$

A number of experimental measurements have indicated that modification of the cross phase can be a large part of transport reduction in L-H transitions

- Tynan, et al. on CCT
- Moyer, et al. on DIII-D
- Boedo, et al. on DIII-D and TEXTOR
- Chapman, et al. on MST (coherence effect?)



- From Boedo, et al.,
PRL 2000
Cross phase between
temperature and electrostatic
potential fluctuations

Results from numerical simulations of turbulence modeling the L-H transition has shown mixed results

- Carreras, et al., : Cross phase strongly modified by ExB shear in simulations of resistive pressure gradient driven turbulence
- Xue, et al., : Cross phase only weakly modified during L-H transitions in edge turbulence modeling

- The evolution of fluctuation amplitudes $\langle \tilde{n}^2 \rangle$ (i.e., an “envelope” equation) has been considered in many models:

$$\frac{d}{dt} = - \frac{dE}{dr}^2$$

- We wish to consider an evolution equation for the cross phase:

$$\frac{d}{dt} \theta_k = \frac{i}{2} \frac{d}{dt} \ln \frac{\langle n_k^* v_k \rangle}{\langle n_k v_k^* \rangle}$$

III. Cross Phase Evolution

- Vorticity equation + density equation:

$$\frac{d}{dt} \tilde{v}^2 + L \tilde{v} = L_n \tilde{n}$$

$$\frac{d}{dt} \tilde{n} + L_{nn} \tilde{n} = L_n \tilde{v}$$



Total time derivatives Direct linear terms Cross linear terms

$$\frac{d}{dt} = \frac{d}{dt} + \underbrace{\langle \mathbf{V}_E \rangle}_{\text{Mean convection}} + \underbrace{\tilde{v} \times \hat{z}}_{\text{Nonlinear convection}}$$

- The terms L , L_n , L_{nn} , L'_n are operators that depend on the model
- Renormalized equations:

$$R_U \tilde{U} = L_n \tilde{n} - L \tilde{} = L_n \tilde{n} - L'_n \tilde{v}_r$$

$$R_n \tilde{n} = L_n \tilde{} - L'_n \tilde{v}_r$$

- Use these to find cross phase equation:

$$\frac{d}{dt} \langle n_k \rangle = \frac{i}{2} \frac{1}{\langle n_k^* v_k \rangle} \frac{d}{dt} \langle n_k^* v_k \rangle - \frac{1}{\langle n_k v_k^* \rangle} \frac{d}{dt} \langle n_k v_k^* \rangle$$

Cross phase evolution equation:

$$\begin{aligned}
 \frac{d}{dt} = & - \left[\overbrace{1 \langle \tilde{n}^2 \rangle}^{\text{Nonlinear phase alignment}} - \overbrace{2 \langle \tilde{n} \rangle}^{\text{Quasilinear phase}} \right] \sin \\
 & + \left[\underbrace{3 \langle \tilde{n}^2 \rangle}_{\text{Nonlinear phase shifts}} + \underbrace{4 \langle \mathbf{V}_E \rangle'^2}_{\text{ExB shear modification}} \right] \cos
 \end{aligned}$$

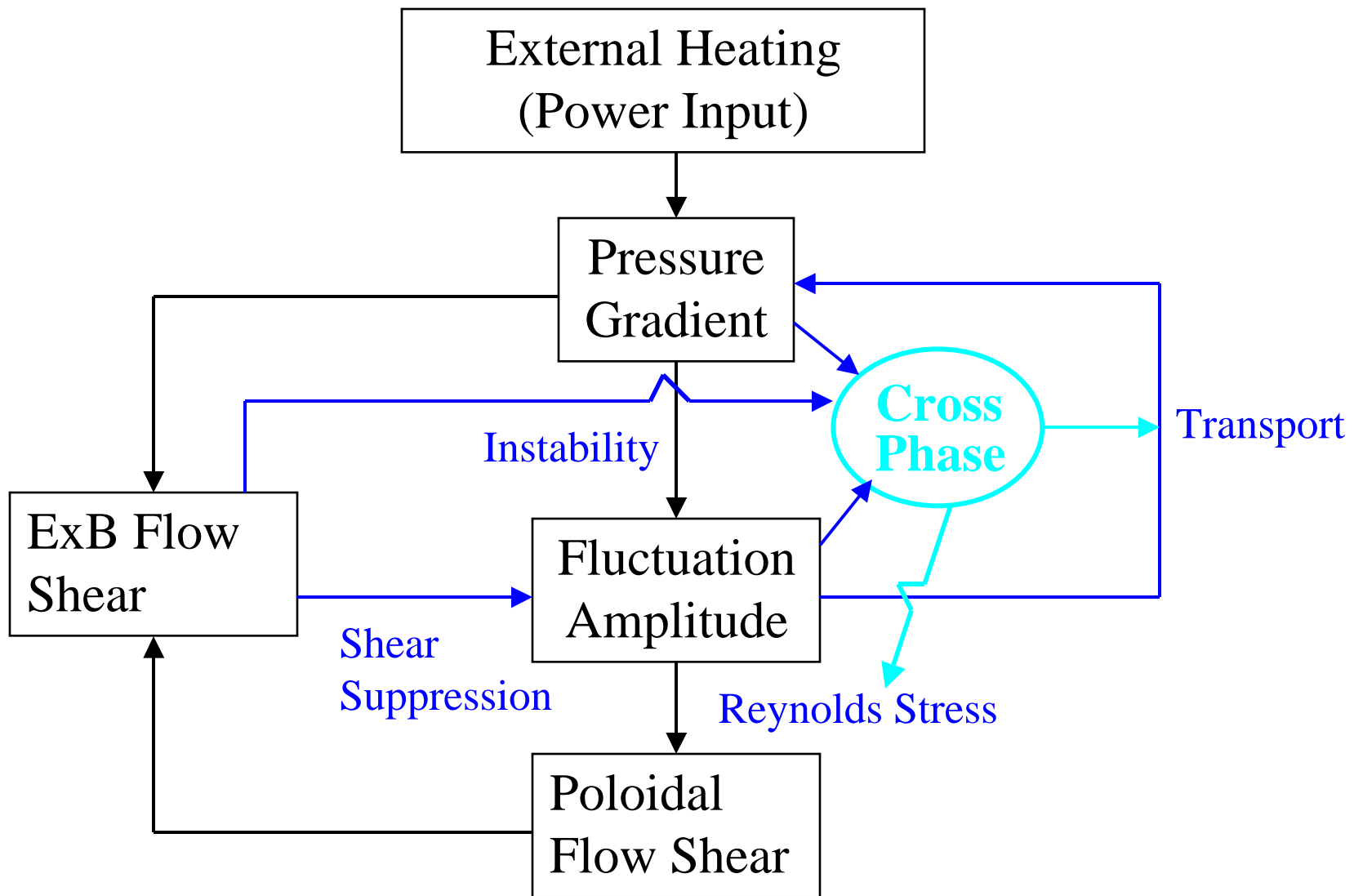
- The coefficients 1 , 2 , and 3 , are all model dependent

Properties of the cross phase equation:

- **Fixed point for the cross phase:**

$$\tan = \frac{\left[3 \langle \tilde{n}^2 \rangle + 4 \langle \mathbf{V}_E \rangle'^2 \right]}{\left[1 \langle \tilde{n}^2 \rangle - 2 \langle \tilde{n} \rangle \right]}$$

- **Nonlinear phase shifts and ExB shear flow tends to move \tilde{n} and \tilde{v}_r out of phase**



Predator-Prey Model with Cross Phase Evolution

(1) Fluctuation Amplitude Evolution:

$$\frac{dE}{dt} = \underbrace{EN}_{\text{Linear instability}} - \overset{\text{Spectral transfer of energy}}{\uparrow} k_1 E^2 (1 + k_8 \cos \) - \underbrace{EU^2}_{\text{Shear suppression}}$$

(2) Poloidal Flow Shear Evolution:

$$\frac{dU}{dt} = \underbrace{k_2 EU}_{\text{Reynolds stress}} (1 + k_9 \cos \) - \overset{\text{Magnetic pumping (Poloidal flow damping)}}{\uparrow} k_3 U$$

(3) Pressure Gradient Evolution:

$$\frac{dN}{d} = \overset{\text{Collisional transport}}{\uparrow} -N - \underset{\text{turbulent transport}}{\downarrow} EN \cos + \overset{\text{Power input}}{\uparrow} Q$$

(4) Radial Force Balance: $U = V - k_{10}N^2$

(5) Cross Phase Evolution:

$$\frac{d}{d} = \overset{\text{Quasilinear phase}}{\uparrow} -k_{11}N \sin - k_{12}E \sin + k_{13}E \cos + \overset{\text{ExB shear modification}}{\uparrow} k_{14}V^2 \cos$$

\downarrow Nonlinear phase alignment \downarrow Nonlinear phase modification

E: Fluctuation Amplitude

N: Pressure Gradient

U: Poloidal Flow Shear

V: ExB Flow Shear

: Cross Phase

Q: Power Input

k_1 - k_{10} : Physical Parameters

All equations are in dimensionless units

- The model has two nontrivial fixed points. Which is stable depends on the input power.
 - At low Q , a fixed point with $U=0$ is stable, this is the “L-mode” like fixed point.
 - At high Q , a fixed point with flow is stable, this is the “H-mode” like fixed point.

Input Parameters:

$k_1: 1$

$k_2: 2$

$k_3: 7$

$Q: 10$

Input Parameters:

$k_1: 1$

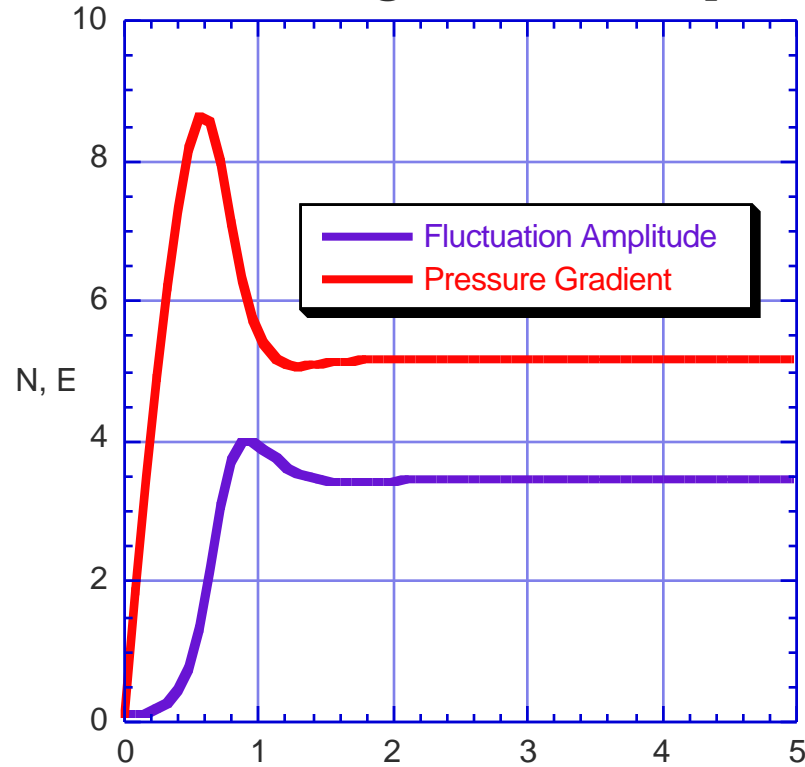
$k_2: 2$

$k_3: 7$

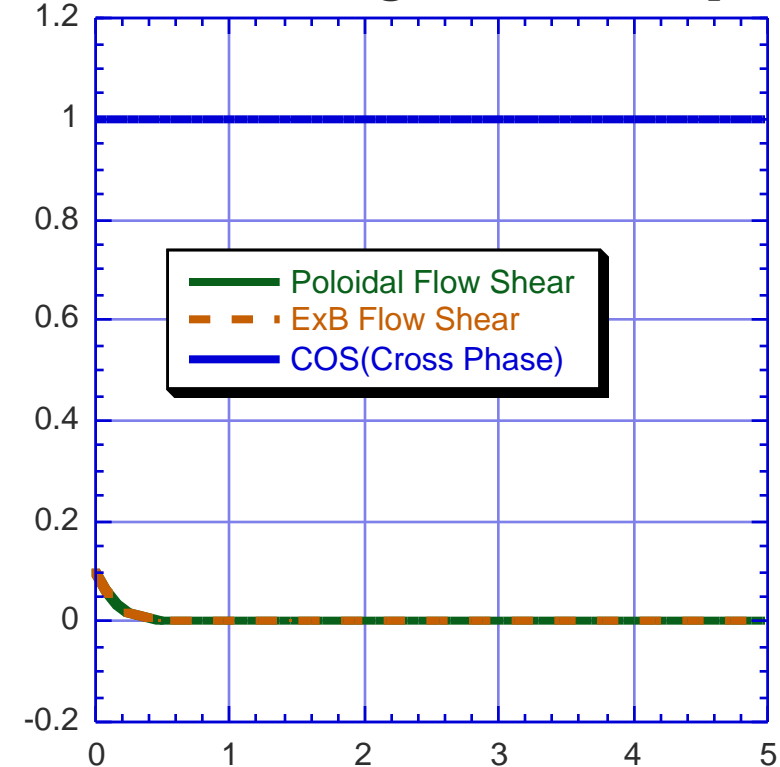
$Q: 24$

An “L-mode” fixed point without cross phase evolution...

Subcritical forcing / Fixed cross phase



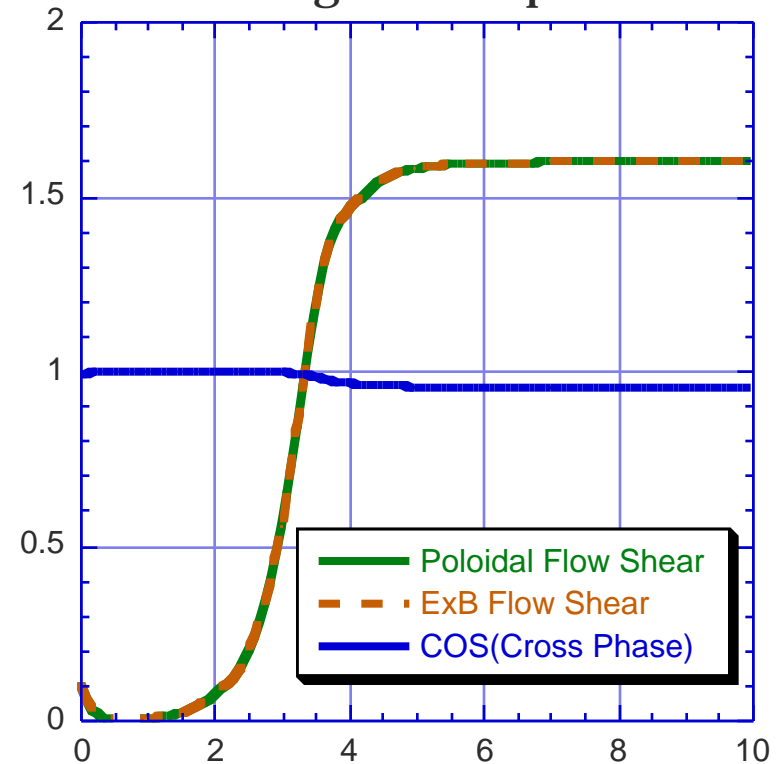
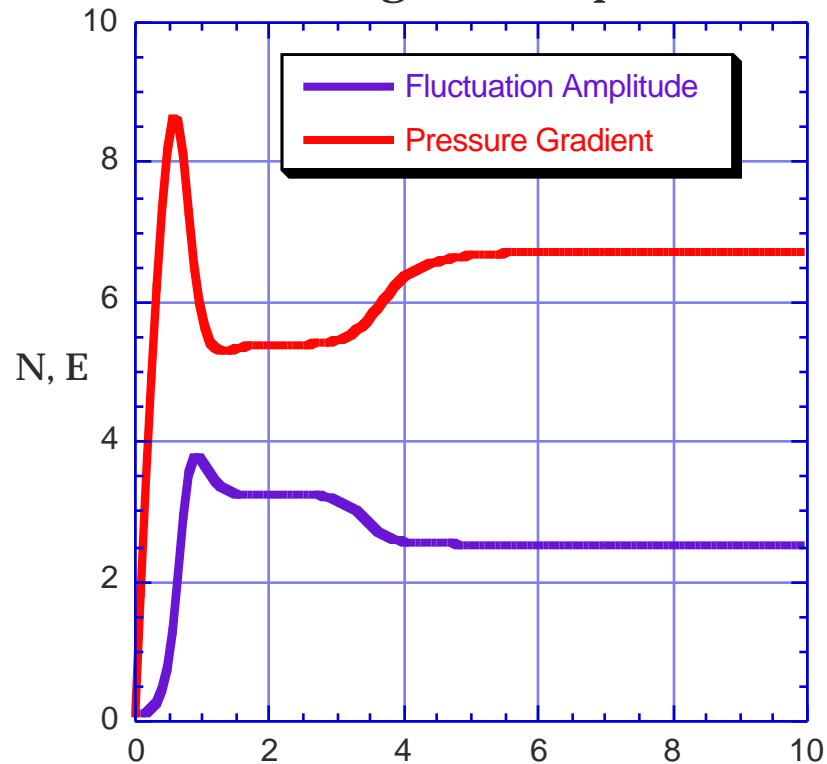
Subcritical forcing / Fixed cross phase



$$k_1=1.5; k_2=2; k_3=7; Q=23$$

...becomes an “H-mode” fixed point with cross phase evolution.

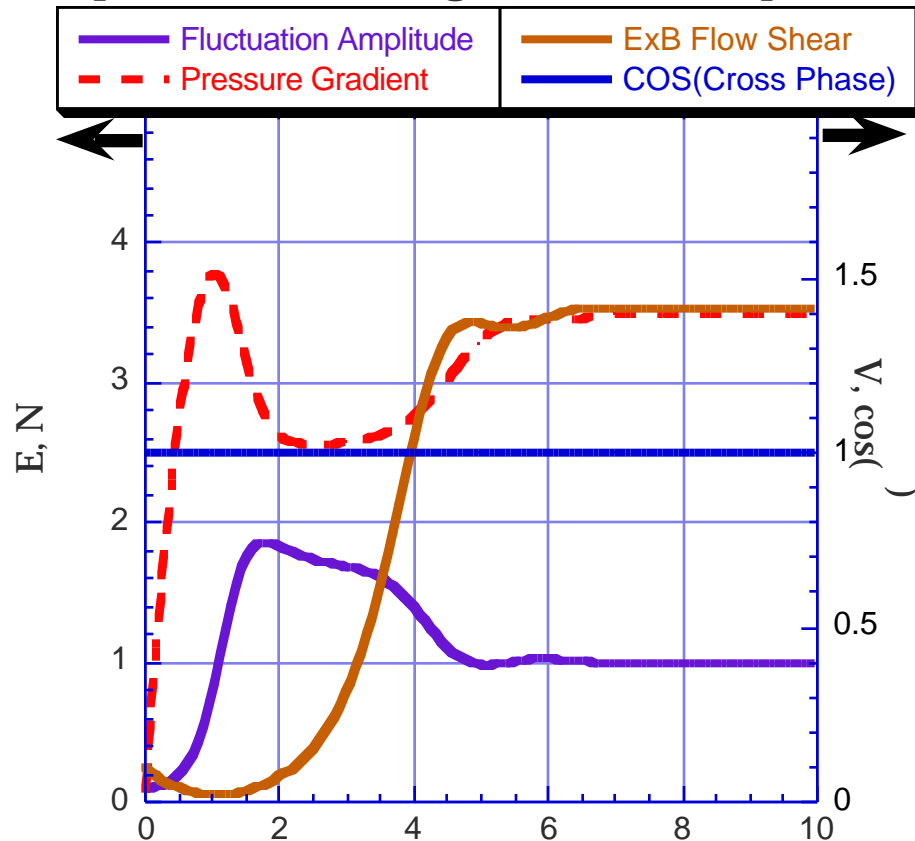
Subcritical forcing / Cross phase evolution Subcritical forcing / Cross phase evolution



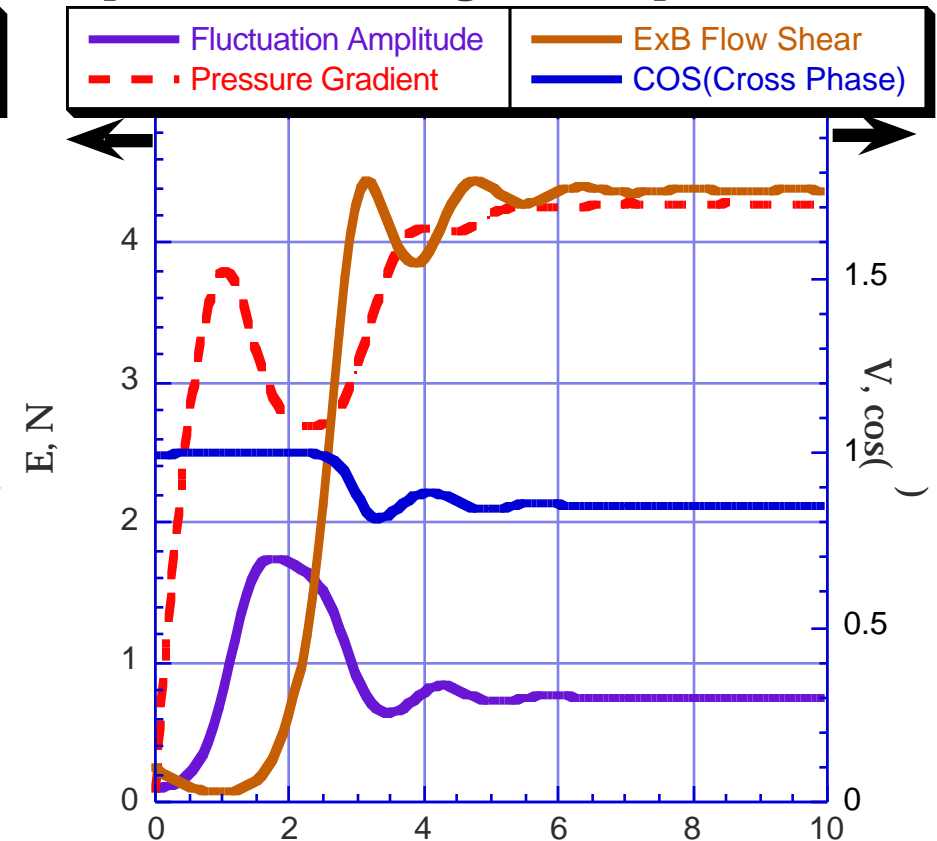
$$k8=0.1; k9=0.4; k10=0; k11=1; k12=1; k13=0.1; k14=1$$

Cross phase effects can also modify the timing of the transition.

Supercritical forcing/ Fixed cross phase



Supercritical forcing/ Cross phase evol.

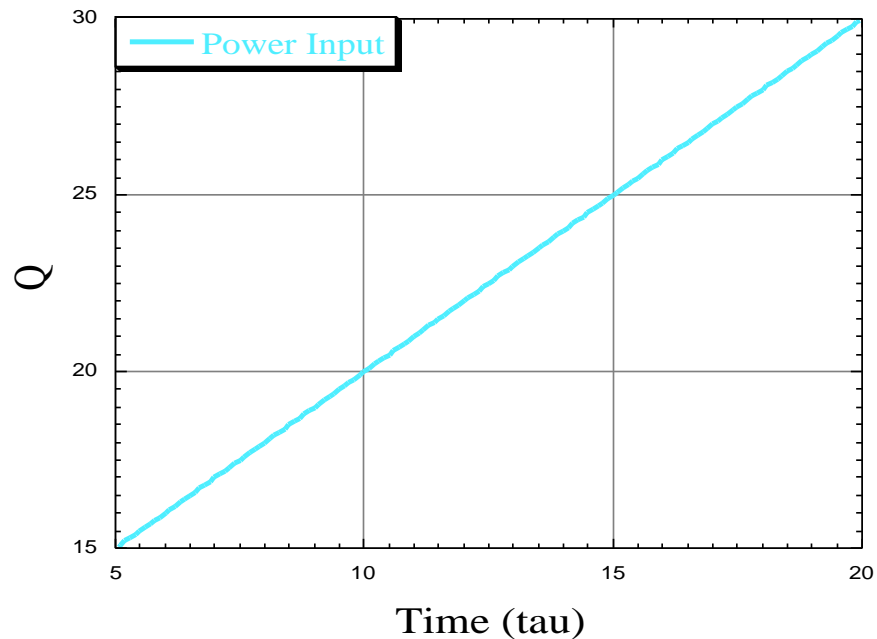


Phase transitions between the two fixed points can be triggered by increasing the power

**Linearly Varying
Power Input:**

$$Q = Q_0 \left(1 + \frac{\tau - 5}{10}\right)$$

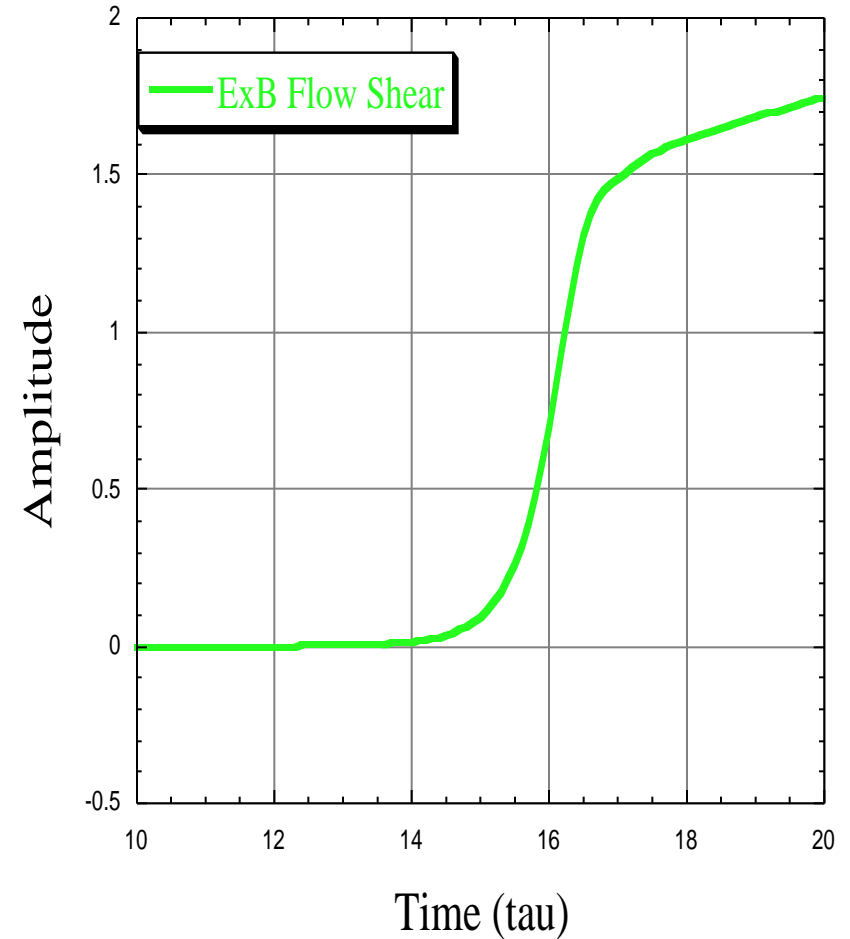
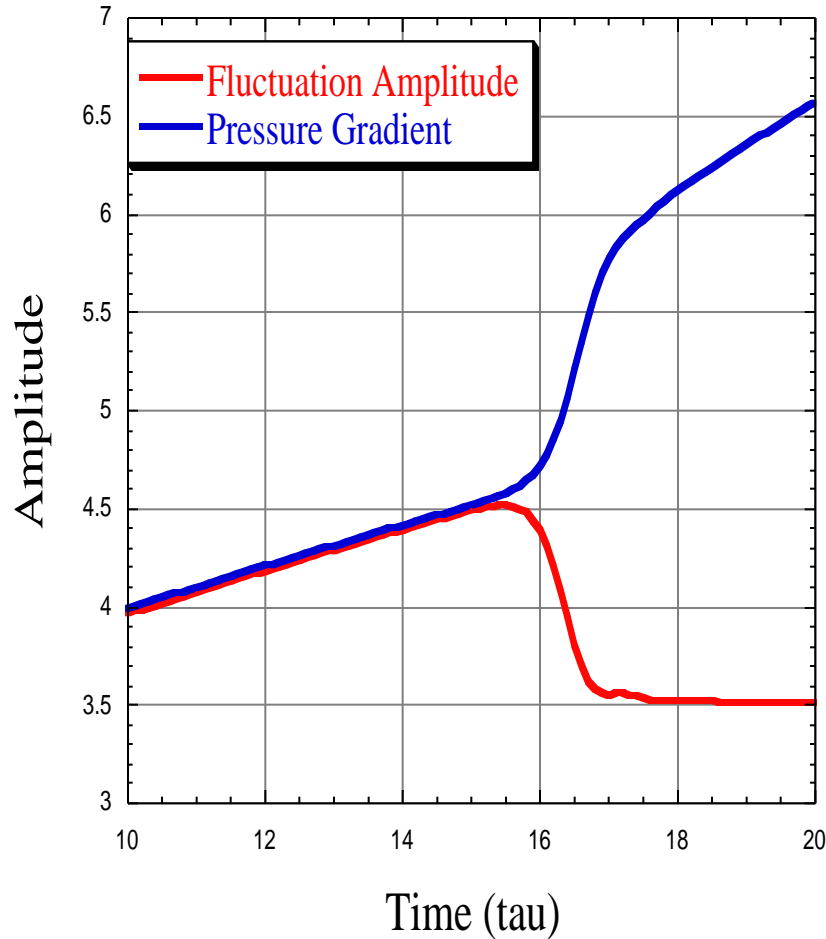
(Same for all cases below)



Input Parameters:

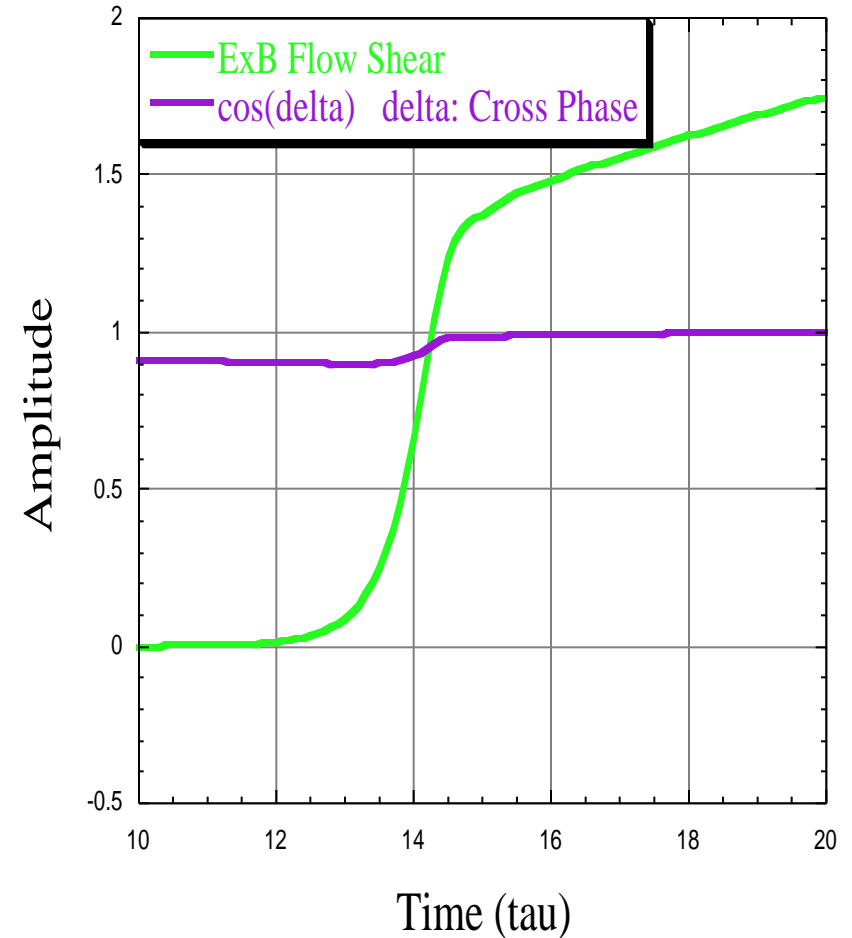
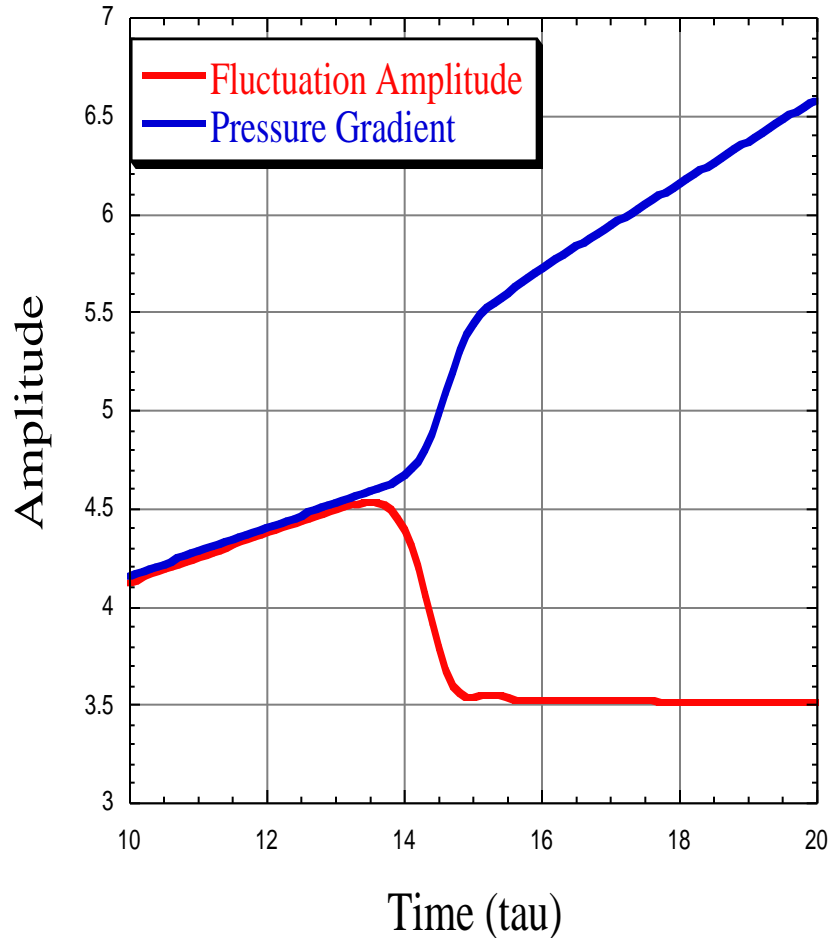
$k_1: 1$ $k_2: 2$ $k_3: 7$ $k_4: 10$ $k_5: 2$ $k_6: 1$ $k_7: 3$ $Q(0): 10$

Predator-Prey Model without Cross Phase



Generation of flow at $\tau = 14$ increases pressure gradient and suppresses fluctuation amplitude. Power threshold $Q = 24$.

Predator-Prey Model with Cross Phase #1



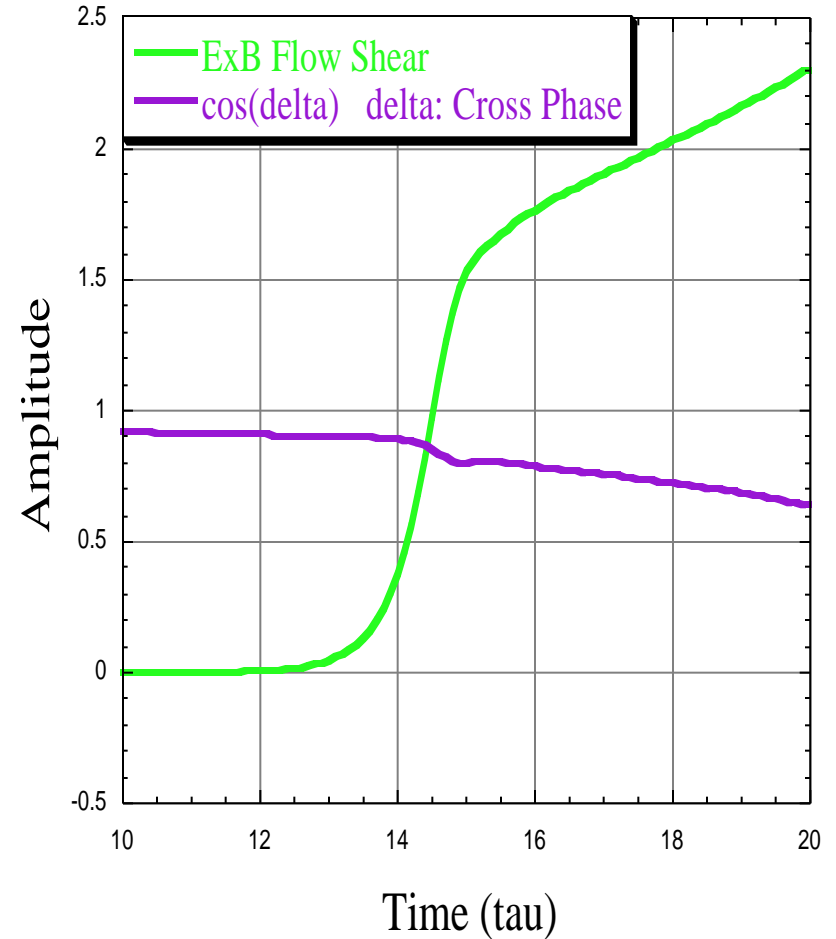
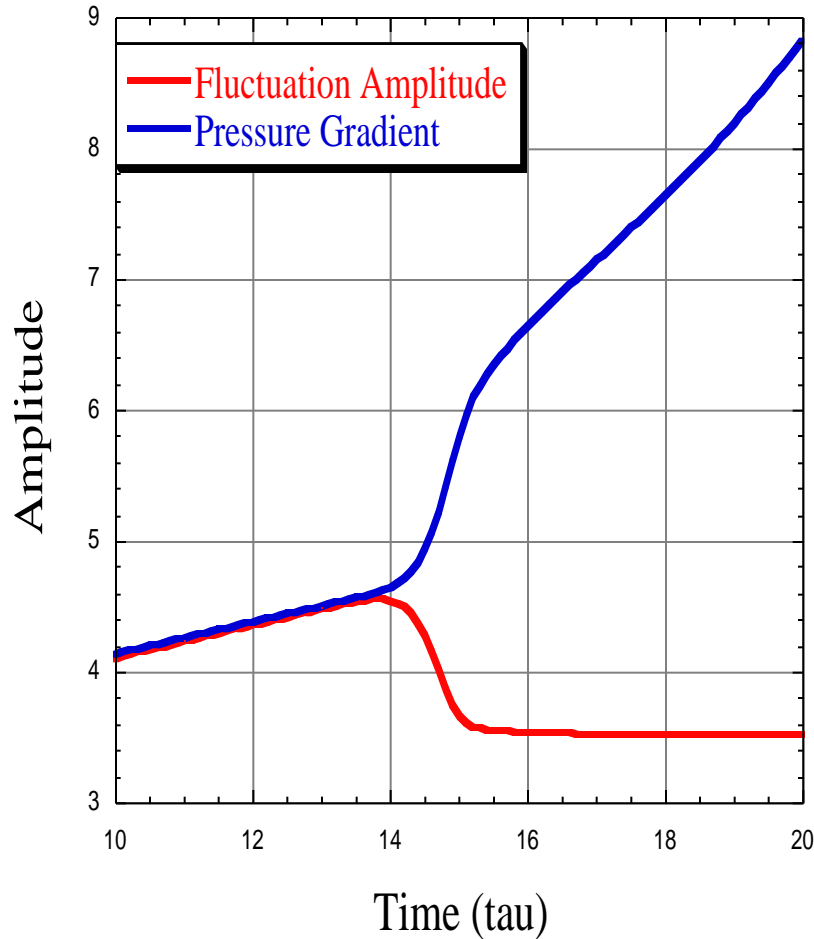
Generation of flow at $\tau = 12$ increases pressure gradient and suppresses fluctuation amplitude. Power threshold $Q = 22$.

If the cross phase is more sensitive to nonlinear modifications, the density gradient increases much more dramatically after the transition

Input Parameters:

$k_1: 1$ $k_2: 2$ $k_3: 7$ $k_4: 10$ $k_5: 2$ $k_6: 3$ $k_7: 3$ $Q(0): 10$

Predator-Prey Model with Cross Phase #2



Generation of flow at $\tau = 12.5$ increases pressure gradient and suppresses fluctuation amplitude. Power threshold $Q = 22.5$.

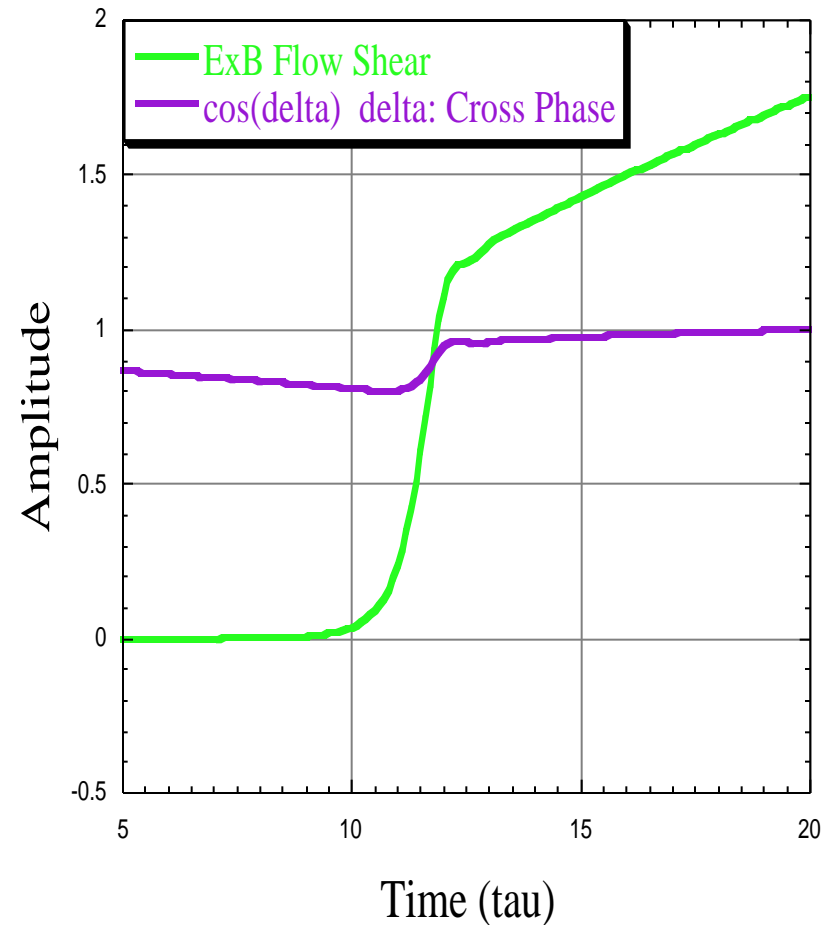
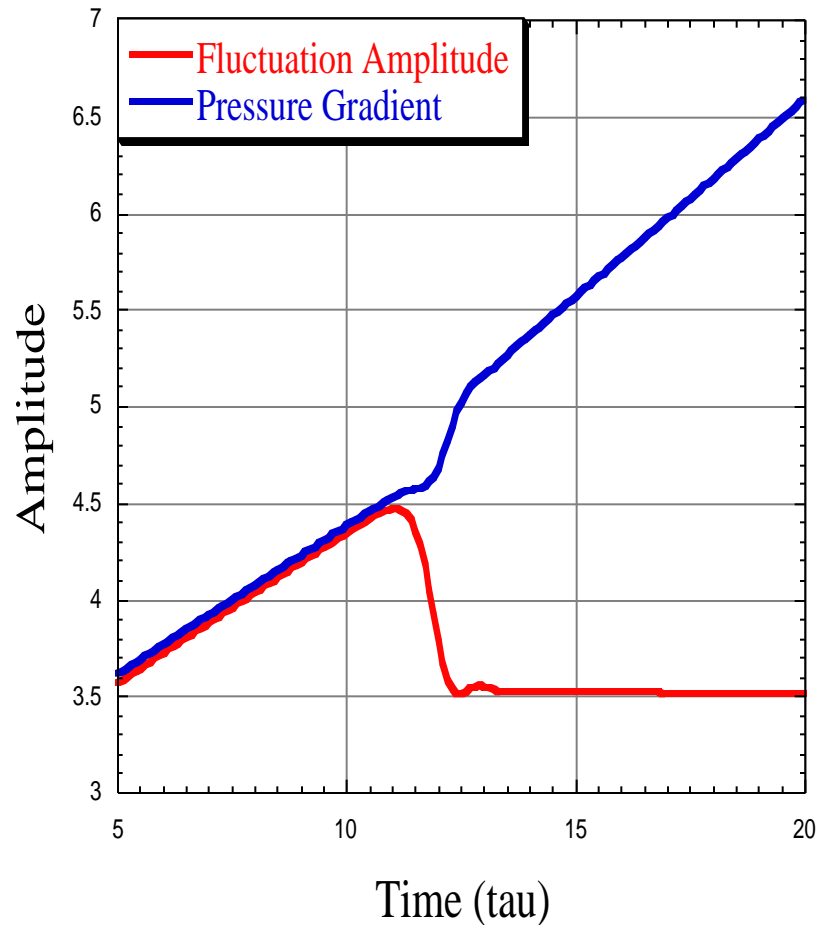
If the cross phase is more easily modified, the power threshold for the transition is lower

Input Parameters:

$k_1: 1$ $k_2: 2$ $k_3: 7$ $k_4: 7$ $k_5: 2$ $k_6: 1$ $k_7: 3$ $Q(0): 10$

- The weight on cross phase in cross phase evolution is increased.

Predator-Prey Model with Cross Phase #3



Generation of flow at $\tau = 9$ increases pressure gradient and suppresses fluctuation amplitude. Power threshold $Q = 19$.

V. Future work

- Look at solutions to the coupled system including cross phase dependence in both flow and density gradient evolution
- Long term possibility is to include cross phase between \tilde{T} and \tilde{v}_r as well
- Derive a better cross phase evolution equation, e.g.

$$\frac{d}{d} = -\left(\cos - 1 + k_6 E + k_7 U^2\right)^2 k_4 N$$